## Lesson 46

## A Laser Diode Beam Converter

This lesson will show how to design the optics to convert a beam from a laser diode into a circular collimated beam. We start with the specs for a typical laser diode, which has a different divergence in $X$ and $Y$. The task is more complicated than a typical beam shaper due to that difference. Here are the data we will work with:

Beam divergence in Y : 8.5 degrees

Divergence in X: 19 degrees
Wavelength: 0.403 um.
We will use the OBG object format, which requires the Gaussian waist radius as a parameter. So we first have to convert the divergence into a radius.

From Section 3.1.2 in the User's Manual, we learn that the program converts the beam radius to a divergence with the formula

$$
\text { DIV = WAV(p) M2 / п } \underline{\text { WAIST No }}
$$

Simple algebra then says that
WAIST = WAV(p) M2 / T DIV No

From this we get GWR $=0.0008644$ in $Y$ and 0.0003868 in $X$. Now we can create a starting RLE file. In the EE editor, type

```
RLE
ID LASER DIODE BEAM CONVERTER
UNI MM
WA1 . }40
OBG 0.0008644 1 .0003868
1 TH }2
2
END
```

Then run this input, and you get a very simple system, our starting point.


It is easy to see how the beam properties in the X direction differ from those in Y :
SYNOPSYS AIPBEAM
ID LASER DIODE BEAM CONVERTER
$13: 43: 50$
GAUSSIAN BEAM ANALYSIS
SURF
BEAM RADIUS WAIST LOCATION

Indeed. The GBR at surface 2 is much smaller in $Y$ than in $X$. Our first job is to even those out.
We have to insert a lens at about the center of the beam shown above. In the WorkSheet, make a checkpoint, and then click the Insert Element button in the WS toolbar. Then click in the PAD display, near the center. The program adds an element.


SYNOPSYS 21-JUL-18 13:44:38

A good first step. Let's look at the beam as it goes through. Type MPE, select the Rotating Perspective option, and show a pattern of a circle around the edge of the beam, in red. Then click Execute.


Spinning the display around, you see the beam in X much larger than in Y , as expected.


Correcting this will require a cylinder lens on surface 3. In WS, select that surface, click the Curvature Dialog button, $\stackrel{(f)}{ }$, then select the Toric or cylinder button and give the $Y-Z$ radius 10 mm and the $X-Z$ radius 0 , making it flat in that direction. Click OK and Close.


Now we have a cylinder on 3 , but we have to adjust it so the beam radius on surface 4 is the same in $X$ and Y . Make a new checkpoint.

Make a new MACro. We don't want the beam too steep (which will be hard to correct), so we ask for thickness 3 to grow to 33 mm .

```
PANT
VY 2 RAD
VY 3 RAD
VY 3 TH
END
AANT
M 33 1 A TH 3
M 7 1 1 A P YA O O 1 O O 4
M 7 1 A P XA 0 1 0 0 4
END
SNAP
SYNO 10
```

After running this, make a new RPER drawing. The beam is indeed circular at 4, as we wanted.


But it is not yet collimated, as we would like. Add another element, with WS, near the end.


We are going to make surface 5 a non-rotationally-symmetric kinoform surface, using shape USS 25. Make a checkpoint, select that surface in WS, and again open the Curvature Dialog. The USS option is
greyed out at the moment, since you have to start with a flat surface to change to any of the USS shapes. So click the FLAT button, and then the USS button. When a new dialog opens, select Type 25 Extended DOE, and click OK and Close.

## Edit Lens Data

$\times$

Enter coefficients to define this uSS surface.

| Coefficient | Function |  |  | $\bigcirc$ Type 1 Power series |
| :---: | :---: | :---: | :---: | :---: |
| 0 | cWav |  |  | $\bigcirc$ Type 2 Power series |
| 0 | ORDER |  |  | $\bigcirc$ Type 3 Fresnel DY |
| 0 | reserued |  |  | $\bigcirc$ Type 4 Fresnel DS |
| 0 | reserved |  |  | $\bigcirc$ Type 5 Power series |
| 0 | reserved |  |  | $\bigcirc$ Type 6 Cosine rings |
| 0 | reserved |  |  | $\bigcirc$ Type 7 Odd powers |
| 0 | reserved |  |  | $\bigcirc$ Type 8 Dual zone |
| 0 | reserved |  |  | $\bigcirc$ Type 9 Forbes A |
| 0 | reserved |  |  | $\bigcirc$ Type 10 Difffuser |
| 0 | HIN |  |  | C Type 11 Forbes B |
| 0 | UNUM |  |  | C Type 12 Forbes c |
| 0 | reserved |  |  | $\bigcirc$ Type 13 Asph. cylinder |
| 0 | reserved |  |  | $\bigcirc$ Type 14 Bezier spline |
| 0 | Y**2 |  |  | $\bigcirc$ Type 15 nurbs surface |
| < |  |  | , | $\bigcirc$ Type 16 simple doE |
|  |  |  |  | $\bigcirc$ Type 17 Biconic Biradial |
|  |  |  |  | $\bigcirc$ Type 18 DLL-defined surface |
|  |  |  |  | $\bigcirc$ Type 19 Y-series surface |
|  |  |  |  | $\bigcirc$ Type 20 Multilayer DOE |
|  |  |  |  | $\bigcirc$ Type 21 Euen and odd powers |
|  |  |  |  | $\bigcirc$ Type 22 Legendre polynomial |
|  |  |  |  | $\bigcirc$ Type 23 Curved Fresnel |
|  |  |  |  | C Type 24 xnurbs |
|  | OK | Cancel |  | - Type 25 Extended DOE |

If you assign a new USS DOE shape, click OK to create default data, and then come back to show them.

This looks like a useful starting system, so let's try to achieve our goals. We want the output to be collimated (which it is not at the moment), so add a surface 7 and make the system AFOCL.

Then make a new MACro:
PANT
VY 2 RD
VY 3 RD
VY 4 RD
VY 3 TH

VY 5 G 16
VY 5 G 17
VY 5 G 18
VY 5 G 19
VY 5 G 20
VY 5 G 21

VY 5 G 24
VY 5 G 25
VY 5 G 26
VY 5 G 27
VY 5 G 28

```
VY 5 G 29
VY 5 G 32
VY 5 G 33
VY 5 G 34
VY 5 G 35
VY 5 G 36
VY 5 G 37
END
AANT
M O 10 A P HH O O 1 O 5
M 7.0 1 A P YA O O 1 0 5
M 7.0 1 A P XA O 1 0 0 5
GNR 0 . 1 9 P
GNO 0 .1 9 P
END
SNAP
SYNO 22
```

This will vary most of the coefficients of the new DOE, keep the beam radius equal to 7 mm in X and Y , ask for the marginal ray to exit with an angle of zero, and correct both transverse and OPD aberrations. The process converges nicely - but element 2 is too thin, so increase the thickness to 3 mm and run the optimization once more. Here is our design:


How well corrected is it? Go to MDI and ask for a pupil plot, scale 0.1 waves/inch. Not bad; less than 1/10 wave of error.

But we're not quite finished. The first element needs a rectangular aperture, and at the moment it has the default circular aperture. We assign the RAO:

```
CHG
2 RAO }8
3 RAO }8
END
```



We haven't said anything about the intensity falloff yet. This is a laser diode, remember, and we assume the intensity profile is Gaussian. Let's check that.

FLUX 20 P 6
Indeed. The flux falls off exactly as we expected. Now we can address the problem of making the profile uniform.

But that is exactly what we did in Lesson 13, so we leave that step as an exercise for the student. Read that lesson and apply the same logic to this case, taking into account the difference in lens construction. If you succeed, you are ready for your diploma. Congratulations.

For reference, the design we did for this lesson is listed below.

| FLUX INTENSITY |  |  |
| :---: | :---: | :---: |
| FLUX AS A FUNCTION OF RELATIVE APERTURE, ON SURFACE 6 <br> THIS ANALYSIS ASSUMES ROTATIONAL SYMMETRY |  |  |
|  |  |  |
| ID LASER DIODE BEAM CONVERTER GAUSSIAN BEAM: $W_{0}=8.64 \mathrm{E}-04 \mathrm{MM} \quad \mathrm{RBS}=1.0000 \mathrm{Wx}=3.87 \mathrm{E}-04 \quad 21-\mathrm{JUL}-18 \quad$ STALPS $\quad 14: 31: 0$ |  |  |


ID LASER DIODE BEAM CONVERTER0.00000000TH 30.13218529 AIR

4 N1 1.62117979
4 GID 'GLM-NdVd
XDD $3-3.7078023 \mathrm{E}-05-2.2003760 \mathrm{E}-06 \quad 3.6721484 \mathrm{E}-08-4.9776438 \mathrm{E}-10 \quad 0.0000000 \mathrm{E}+00$
XDD $4 \quad 0.0000000 \mathrm{E}+00-7.0629761 \mathrm{E}-02-4.0279060 \mathrm{E}-05 \quad 5.1724603 \mathrm{E}-07-6.0078137 \mathrm{E}-05$
XDD $5 \quad 1.4720853 \mathrm{E}-06-1.2222347 \mathrm{E}-08 \quad 0.0000000 \mathrm{E}+00 \quad 0.0000000 \mathrm{E}+00 \quad 0.0000000 \mathrm{E}+00$
END

